**INTRAPARTICLE DIFFUSION-ADSORPTION MODEL TO DESCRIBE LIQUID/SOLID ADSORPTION KINETICS****MODELO DE DIFUSIÓN-ADSORCIÓN INTRAPARTÍCULA PARA DESCRIBIR CINÉTICAS DE ADSORCIÓN LÍQUIDO/SÓLIDO**

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Abstract

The most popular formula used in the literature about liquid/solid adsorption kinetics to describe diffusion-controlled processes is the intraparticle diffusion (IPD) equation. However, this formula was introduced originally for pure diffusion. It does not account explicitly for the effect of adsorption (except in the limit of very low adsorbate concentration). In this work, the problem of diffusion-controlled kinetics is studied by using a diffusion-adsorption model which should hold when the solute concentration in the external solution is sufficiently high. The case of a finite amount of solute initially in the stirred batch adsorber is solved analytically. For short times, the formula for the uptake turns out to have the same form vs. time as the IPD equation. However, it also predicts a decrease of the fractional uptake with the initial bulk concentration, as observed in the literature, and it shows that the IPD diffusion coefficient is a lumped parameter depending on the experimental conditions. These theoretical results are used for a discussion of the IPD equation and for descriptions of experimental results taken from the literature.

Keywords: adsorption, kinetics, shrinking core model, intraparticle diffusion equation.

Resumen

La fórmula más popular utilizada en la literatura sobre cinética de adsorción líquido/sólido para describir procesos controlados por la difusión es la ecuación de difusión intrapartícula (DIP). Sin embargo, esta fórmula se introdujo originalmente para difusión pura. No toma en cuenta de forma explícita el efecto de la adsorción (excepto en el límite de concentración adsorbida muy baja). En este trabajo, el problema de la cinética controlada por la difusión se estudió mediante el uso de un modelo de difusión-adsorción, que debe ser válido cuando la concentración del soluto en la solución externa es bastante alta. El caso de una cantidad finita de soluto inicialmente en el baño de solución está resuelto analíticamente. Para tiempos cortos, la fórmula para la adsorción resulta tener la misma forma en función del tiempo como la ecuación DIP. Sin embargo, predice una disminución de la fracción de adsorción con una concentración inicial mayor, lo que ha sido observado experimentalmente en la literatura, y enseña que el coeficiente de DIP es un parámetro agrupado que depende de las condiciones experimentales. Estos resultados teóricos son utilizados para una discusión de la ecuación DIP y para descripciones de resultados experimentales tomados de la literatura.

Palabras clave: adsorción, cinética, modelo de núcleo contraído, ecuación de difusión intrapartícula.

1 Introduction

Sorption is of great value for the purification of waters and industrial effluents containing contaminants or pollutants. The modeling of the kinetics is important for the prediction of uptake rates and for gaining more insight into the mechanisms. However, this is still a discussed problem (Qiu *et al.*, 2009). Moreover, a particular situation prevails in this field, which may be viewed as follows.

It has long been recognized that most sorption

processes in macroscopic adsorbent beads are controlled by diffusion in the particles, or in a layer at the periphery of the particles (Ruthven, 1984; Do, 1998). Apparently (Do, 1998), this hypothesis was put forward for the first time nearly one century ago by McBain on the basis of experiments with carbon (McBain, 1919). It was also first recognized by Boyd (Boyd *et al.*, 1947) in the case of ion exchange (Liberti and Helfferich, 1983). In an article published in 1965, Helfferich started by stating: "It has long been known that ion-exchange rates are controlled by diffusion"

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(Helfferich, 1965).

Consequently it is surprising that descriptions of experimental results based on a rate-limiting equation for the adsorption reaction have become increasingly popular in the past 30 years (Ho and McKay, 1999). These empirical equations include the pseudo-first-order (Lagergren, 1898) and the pseudo-second-order rate law (Blanchard *et al.*, 1984; Gosset *et al.*, 1986). Other more physical descriptions assumed a mixed regime combining diffusion and local adsorption reaction (Wen, 1968; Yang and Al-Duri, 2001; Che-Galicia *et al.*, 2014; Castillo-Araiza, 2015).

The other formula that is usually tested against the chemical rate laws is the “intra-particle diffusion” (IPD) equation (Kushwaha *et al.*, 2010; Boparai *et al.*, 2011; Tofighy and Mohammadi, 2011) which is supposed to be relevant in the case of diffusion-controlled sorption processes (Weber and Morris, 1963; Rudzinski and Plazinski, 2008; Wu *et al.*, 2009; Haerifar and Azizian, 2013). This equation was first employed by Boyd *et al.* in 1947 (Boyd *et al.*, 1947) to model ion exchange kinetics in zeolites. However, this formula was established originally to describe pure free diffusion of a solute in a sphere (see for instance Eq. (6.20) of (Crank, 1975)). It does not account explicitly for the effect of adsorption.

In the present work we focus on diffusion-controlled adsorption processes and propose to revive a model that takes into account the influence of adsorption on solute transport in the adsorbent. This model was first proposed in the seminal work by Crank (Crank, 1957, 1975). When applied to sorbent spherical beads, it is an example of the well-known so-called “shrinking unreacted core” model (Yagi and Kunii, 1961; Ruthven, 1984; Levenspiel, 1999; Leyva-Ramos *et al.*, 2010, 2012, 2015) in which adsorption of the diffusing solute progressively builds up an ash shell of reacted material at the periphery of the bead and leaves an unreacted core at the centre, that shrinks in the course of time. The model introduced by Crank was solved in the case of a very large (virtually infinite) amount of solute, in which the external solution concentration could be taken as constant (Crank, 1957, 1975; Ruthven, 1984; Levenspiel, 1999). In practice, this model should be applicable when the solute concentration in the batch adsorber is sufficiently large (see section 2).

In this paper, we first recall briefly the main ingredients and results of the model in one dimension (1D). The method used here serves to gain more insight into the main features of the process. Next, the model is solved in the case of spherical beads for

a finite amount of adsorbate present initially in the batch adsorber, in which case its bulk concentration varies with time. The result is used to derive a formula valid at short contact times, for particles of arbitrary (but smooth) shape, and for a discussion of the IPD equation. It is shown that the diffusion coefficient introduced in the IPD equation is in fact a lumped parameter that, besides diffusion, also includes the effect of the experimental conditions. The conditions required for applying the model to real experiments are discussed. The obtained formulas are utilized to describe experimental data taken from the literature.

2 Modeling

2.1 Ingredients of the model

We consider an adsorbent medium (denoted by A) in contact with a perfectly stirred batch adsorber, denoted by B, containing all of the solute initially. The adsorbate diffuses freely in A until it is immobilized when it encounters a free site.

As shown in the literature (Ruthven, 1984; Grathwohl, 2012), in the case of very low concentration of solute, the latter obeys a diffusion equation with an effective diffusivity, $D_{eff} = D(1 + \alpha)$ (Ruthven, 1984; Grathwohl, 2012), in which D is the diffusivity of free solute and α is the slope of the adsorption isotherm for very low concentration.

On the opposite, in the present work, the initial concentration in the batch adsorber will be sufficiently high so that the ash layer of the adsorbent operates in the plateau region of the adsorption isotherm. In this case, the degree of adsorption in the reacted zone will not vary appreciably in the course of time as long as the external concentration remains high enough.

In the model, the medium will be considered to possess a uniform concentration of sites, denoted by C_s , onto which the solute molecules form a monolayer. It will be supposed that the adsorption process is diffusion-controlled, i.e. the adsorption process is very fast compared to diffusion. The latter will be described by using an average diffusion coefficient in A, which will account for the various possible diffusion pathways in the medium (micropore, mesopore, macropore, and surface diffusion (Do, 1998)). The total amount of solute will be sufficiently high so that the ash layer thickness in A at equilibrium is not very small. So, the concentration of solute on the surface of A will be taken equal to that in the batch adsorber, denoted by C_B . The boundary condition for the solute

concentration in A will be that the concentration of free solute is continuous at the mouth of a pore.

The classic quasi-steady state (QSS) approximation (Briggs and Haldane, 1925; Kramers, 1940; Crank, 1975; Simonin *et al.*, 1991) will be used to derive analytical results. Generally, the QSS regime does not hold at the very beginning of the process, but it settles after a short induction time.

2.2 Adsorption in a semi-infinite slab (1D case)

Before examining the spherical case, it is useful to first present shortly the model introduced by Crank (Crank, 1957, 1975) in the one-dimensional (1D) case and solve it in the QSS approximation because this has not been done before in the literature and some results will then be used for the spherical case. Moreover this derivation gives more insight into the process.

We consider a semi-infinite porous slab of adsorbent that is put in contact at $t = 0$ with a very large bath of batch adsorber of constant concentration, $C_B^{(0)}$ (see Fig. 1). When the solute diffuses in A in the direction x perpendicular to the surface of A, it binds to free sites and progressively builds up a reacted zone in which all adsorption sites are occupied. We denote by δ_1 the thickness of this ash layer in 1D.

The concentration of free solute, $C(x, t)$, in this zone obeys Fick's second law which reads $\partial C(x, t)/\partial t = -\partial J(x, t)/\partial x = D\partial^2 C(x, t)/\partial x^2$, with t the time, D the diffusion coefficient of the adsorbate in A, and J the flux of solute molecules per unit cross-section area given by Fick's first law, $J(x, t) = -D\partial C(x, t)/\partial x$. It results from the definition of δ_1 that $C = 0$ at $x = \delta_1$.

The variation of δ_1 in a time interval dt is given by the relation,

$$C_s [\delta_1(t + dt) - \delta_1(t)] = J(x = \delta_1, t) dt \quad (1)$$

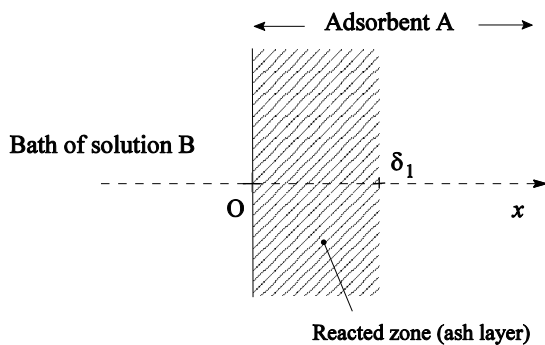


Fig. 1. Sorption in a flat slab.

which expresses the fact that the variation of the number of occupied sites in the lapse of time dt is equal to the number of solute molecules arriving at the position $x = \delta_1$ at time t . At this location, the adsorbent acts like a sink for the solute.

In the QSS approximation one has, $\partial C(x, t)/\partial t \approx 0$ in the ash layer (and $C = 0$ for $x > \delta_1$). Then $J(x, t)$ is approximately constant in space in this layer by virtue of Fick's second law, so that $J = J(t)$. Consequently, the concentration profile is approximately linear in this zone because of Fick's first law. Because of the boundary condition, $C = pC_B^{(0)}$ at $x = 0^+$, J is therefore given by,

$$J(t) \approx D \frac{pC_B^{(0)}}{\delta_1(t)} \quad (2)$$

By combining Eqs. (1) and (2) one gets the equation,

$$C_s \frac{d\delta_1}{dt} = D \frac{pC_B^{(0)}}{\delta_1(t)} \quad (3)$$

which yields,

$$\delta_1(t) = \sqrt{2aD_0t} \quad (4)$$

with

$$a \equiv \frac{C_B^{(0)}}{C_s} \quad (5)$$

and

$$D_0 \equiv pD \quad (6)$$

the effective diffusion coefficient in the porous adsorbent. In what follows it will be taken as a constant because the solute concentration will be very low (see Results and discussion section). The total uptake of solute by A (per unit cross-section area) is

$$Q \approx C_s \delta_1 \quad (7)$$

because in practical applications one may neglect the concentration of free solute in A as compared to that of adsorbed solute. Therefore one gets from Eqs. (4)-(7),

$$Q \approx C_B^{(0)} \sqrt{2D_0t/a} = \sqrt{2C_B^{(0)} C_s D_0 t} \quad (8)$$

We notice that in this relation Q varies as $\sqrt{C_B^{(0)}}$. It is not proportional to $C_B^{(0)}$. This point is further discussed below in section 2.4.

2.3 Adsorption in spherical beads

We now consider sorbent spheres of radius R that are immersed at $t = 0$ in a well-stirred batch adsorber of initial concentration $C_B^{(0)}$. In general, the particles used in adsorption experiments may be

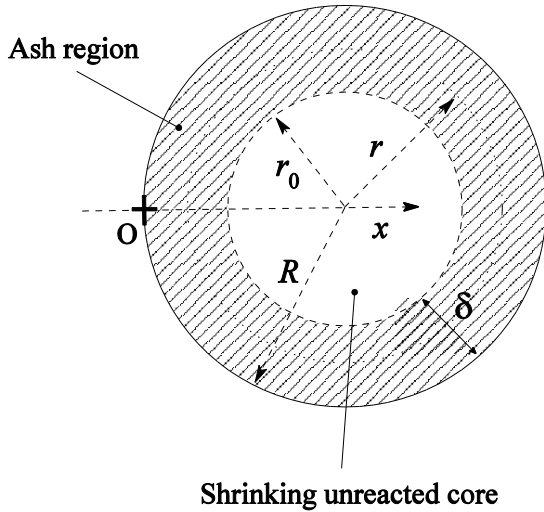


Fig. 2. Sorption into a sphere.

represented by spheres with a good accuracy (Ruthven, 1984). They will typically be made of a porous material like activated carbon.

In this section, we use the same type of model as in the 1D case. Its application to adsorption in spheres has been solved in the literature in the case of an infinitely large amount of solution, in which the adsorbate concentration remained constant (Crank, 1957, 1975; Levenspiel, 1999). It is solved below in the case of a finite amount of adsorbate, whose bulk concentration varies with time.

Let us define the maximum site occupancy ratio of a sphere as the ratio of the total number of solute molecules to the total number of sites,

$$\rho \equiv \frac{C_B^{(0)} V_B}{C_s v} = a \frac{V_B}{v} \quad (9)$$

with v the volume of a sphere and V_B the volume of batch adsorber per sphere (volume of the bath divided by the number of spheres).

A spherical bead is depicted in Fig. 2. We denote by r_0 the position of the moving boundary delimiting the shrinking unreacted core, at which the concentration of free solute concentration vanishes, and by δ the thickness of the ash (reacted) shell.

The free solute concentration at position r and time t , $C(r, t)$, obeys Fick's law, $\partial u / \partial t = D \partial^2 u / \partial r^2$, with $u \equiv rC(r, t)$ (Crank, 1975). The QSS approximation in the sphere reads: $\partial u / \partial t \approx 0$. Then, using the latter relation and the boundary condition, $C(r = R^-, t) = pC_B$, and solving Fick's law one obtains,

$$C(r, t) = \frac{R}{R - r_0} \left(1 - \frac{r_0}{r}\right) pC_B \quad (10)$$

The relation for the time variation of r_0 , similar to Eq. (1), reads,

$$\frac{dn}{dt} = -4\pi r_0^2 J(r = r_0, t) = -C_s \frac{d(\frac{4}{3}\pi r_0^3)}{dt} = -C_s (4\pi r_0^2) \frac{dr_0}{dt} \quad (11)$$

in which n is the number of moles of solute arriving at r_0 and the flux per unit cross-section area is given by $J = -D \partial C / \partial r$.

It stems from Eqs. (10) and (11) after a simple manipulation that,

$$-D_0 \frac{C_B}{C_s} dt = r_0 \left(1 - \frac{r_0}{r}\right) dr_0 \quad (12)$$

in which C_B is obtained from the conservation of total solute amount in the course of time: $C_B^{(0)} V_B = C_B V_B + Q$, with Q the amount of adsorbed solute,

$$Q = \frac{4}{3}\pi (R^3 - r_0^3) C_s \quad (13)$$

in which we also used Eq. (7). Then one gets,

$$C_B = C_B^{(0)} \frac{\rho + z^3 - 1}{\rho} \quad (14)$$

in which we have used Eq. (9) and introduced the non-dimensional radius of the core,

$$z \equiv \frac{r_0}{R} \quad (15)$$

Insertion of Eq. (14) into Eq. (12) gives the following separable differential equation obeyed by z ,

$$\frac{D_0 a}{R^2} dt = -z(1 - z) \frac{\rho}{\rho + z^3 - 1} dz \quad (16)$$

with a defined by Eq. (5). The two sides of this equation can be integrated separately (e.g. with the help of Maple), between the states ($t = 0, z = 1$) and ($t, z(t)$). After some rearrangements of terms, one arrives at the following result,

$$\tau = \frac{2(1 - \lambda^3)(1 - \lambda)}{\lambda} \ln \left(\frac{1 - \lambda}{z - \lambda} \right) + \frac{(1 - \lambda^3)(2\lambda + 1)}{\lambda} \ln \left(\frac{z^2 + z\lambda + \lambda^2}{1 + \lambda + \lambda^2} \right) + \frac{2\sqrt{3}(1 - \lambda^3)}{\lambda} \arctan \left[\frac{\sqrt{3}\lambda(1 - z)}{z(\lambda + 2) + \lambda(2\lambda + 1)} \right] \quad (17)$$

in which

$$\tau \equiv 6 \frac{a D_0}{R^2} t \quad (18)$$

is a non-dimensional reduced time, and the parameter λ defined by,

$$\lambda \equiv (1 - \rho)^{1/3} \quad (19)$$

has been introduced for convenience. In practice, one generally has $\rho < 1$. Then it is easy to show that the minimum value of z satisfies the relation, $\rho = 1 - z_{\min}^3$, from which one gets using Eq. (19),

$$z_{\min} = \lambda \quad (20)$$

which expresses the concrete meaning of the parameter λ .

The fractional uptake (proportion of solute immobilized in the sphere) is (Do, 1998),

$$P \equiv \frac{Q}{C_B^{(0)} V_B} \quad (21)$$

By using Eqs. (9), (13) and (15) in Eq. (21) one gets,

$$P = \frac{1 - z^3}{\rho} \quad (22)$$

from which it stems that,

$$z = (1 - \rho P)^{1/3} \quad (23)$$

Therefore, τ can be expressed as a function of P and ρ alone by inserting Eqs. (19) and (23) into Eq. (17).

2.4 Formula at short times

For small diffusion times, P is small. In that case, one gets from Eq. (23) that $z \approx 1 - \rho P/3$, which relation may be inserted into Eq. (17). A Taylor expansion of this expression for τ to the second order in powers of P leads to $P \approx \sqrt{3\tau}/\rho$, which may be rewritten using Eq. (18) as,

$$P \approx \frac{1}{R} \sqrt{18 \frac{aD_0}{\rho^2} t} \quad (24)$$

or, together with Eqs. (5) and (9),

$$P \approx \frac{1}{R} \frac{v}{V_B} \sqrt{18 \frac{C_s}{C_B^{(0)}} D_0 t} \quad (25)$$

In fact, Eq. (25) may be obtained in another way, by noting that for small contact times the solute is adsorbed in a shell of small thickness given by the formula in 1D (Eq. (4)) and area $4\pi R^2$, so that, $Q \approx C_s 4\pi R^2 \delta_1$, which together with Eq. (21) leads to Eq. (24) or (25).

Moreover, as a consequence, we notice that this treatment may be applied to particles of arbitrary, yet

smooth, shape in the first moments of the process. Then, the amount of solute adsorbed in the particle is given by,

$$Q \approx C_s A \delta_1 = A \sqrt{2C_s C_B^{(0)}} \sqrt{D_0 t} \quad (26)$$

with A the area of the particle, and consequently,

$$P \approx \frac{A}{V_B} \sqrt{2 \frac{C_s}{C_B^{(0)}}} \sqrt{D_0 t} \quad (27)$$

An important result of this latter formula is that the fractional uptake, P , not only varies as $t^{1/2}$. It is also noticed that P should decrease with $C_B^{(0)}$ as $1/\sqrt{C_B^{(0)}}$ (for constant C_s), which is not a trivial result. This is due to the fact that the adsorbed amount, Q (which increases with $C_B^{(0)}$ as expected, see Eq. (26)), varies as $\sqrt{C_B^{(0)}}$, because the ash layer thickness, δ_1 , varies in this way (Eq. (4)). This property clearly distinguishes a diffusion-controlled adsorption process from a simple pure diffusion process, for which P is independent of $C_B^{(0)}$.

2.5 Intraparticle diffusion equation

The classic intraparticle diffusion (IPD) equation (Boyd *et al.*, 1947; Weber and Morris, 1963; Rudzinski and Plazinski, 2007; Wu *et al.*, 2009) in the case of a sphere is expressed as,

$$P_{IPD}(t) \equiv \frac{Q_{IPD}(t)}{Q_B^{(0)}} = 1 - \frac{6}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{n^2} \exp(-n^2 \pi^2 D_{IPD} t / R^2) \quad (28)$$

in which P_{IPD} is the fractional uptake of solute, Q_{IPD} is the uptake, $Q_B^{(0)}$ is the initial amount of solute in B ($Q_B^{(0)} \equiv C_B^{(0)} V_B$), and D_{IPD} is an ad hoc diffusion coefficient. Eq. (28) was written in such a way that the uptake satisfies the two conditions: $Q_{IPD}(t = 0) = 0$, and $Q_{IPD}(t = \infty) = Q_B^{(0)}$.

It seems that this relation was first used by Boyd *et al.* (1947) to describe adsorption kinetics in zeolites. However, as said previously, it does not take into account explicitly the effect of adsorption. It is the solution to the problem of free diffusion of a solute from a batch adsorber of constant concentration into a sphere that does not possess adsorption sites (Eq. (6.20) of (Crank, 1975)).

At the beginning of the process, Eq. (28) may be approximated by the following equation (Crank, 1975;

Rudzinski and Plazinski, 2007),

$$P \approx \frac{6}{R} \sqrt{\frac{D_{IPD}}{\pi} t} \quad (29)$$

In the literature, the IPD equation has generally been used in the latter form preferentially to the full formula, Eq. (28). It is worth noting that Eq. (29) coincides with the result from the present model, Eq. (24), that is $P_{IPD} \approx P$ at short times, provided that the diffusion coefficient appearing in the IPD equation satisfies the relation,

$$D_{IPD} = \frac{\pi a}{2 \rho^2} D_0 \quad (30)$$

or, by using Eqs. (25) and (29),

$$D_{IPD} = \frac{\pi C_s}{2 C_B^{(0)}} \left(\frac{v}{V_B} \right)^2 D_0 \quad (31)$$

This result shows that the IPD diffusion coefficient is in fact a lumped parameter which depends on the experimental conditions. In particular, within the present model, for a given type of sorbent particles and a given volume of bath per particle, this pseudo-diffusion coefficient is expected to be inversely proportional to $C_B^{(0)}$. We note that a decrease of D_{IPD} with the initial bulk solute concentration has often been reported in the literature, e.g. in (Kumar *et al.*, 2003; Rudzinski and Plazinski, 2007, 2008).

When D_{IPD} is given by Eq. (30), then $P_{IPD} \approx P$ at short times, but P_{IPD} becomes larger than P for longer times. It was observed that the maximum deviation grows with the value of ρ . It reaches 7.2% for $\rho = 0.1$, ca. 13% for $\rho = 0.5$ and ca. 20% for $\rho = 0.9$.

2.6 Application of the model to experiments

The value for the concentration of sites, C_s , to be taken in the model must be determined. To illustrate, let us assume that the adsorption isotherm of A may be parameterized using the Langmuir equation, which is generally written as,

$$q_a = \frac{K_L C_B^{(eq)}}{1 + a_L C_B^{(eq)}} \quad (32)$$

with q_a the amount of solute adsorbed in A per mass unit of A, $C_B^{(eq)}$ the concentration of solute in the bath in equilibrium with the sorbent, and K_L and a_L parameters that are characteristic of the adsorbent.

This relation may be rewritten in the following different form,

$$q_a = \frac{C_B^{(eq)}}{C_B^{(eq)} + C_{1/2}} q_{sat} \quad (33)$$

with $q_{sat} = K_L/a_L$ the amount at saturation and $C_{1/2} = 1/a_L$. This form expresses the fact that $q_a = q_{sat}/2$ for $C_B^{(eq)} = C_{1/2}$, and $q_a \sim q_{sat}$ when $C_B^{(eq)} \gg C_{1/2}$.

If the adsorption process is sufficiently fast, one may assume a local equilibrium in a pore between the free solute and the solute adsorbed on the wall of the pore. Then, Eq. (33) may be extended to express the space-averaged concentration of adsorbed solute at a position in a pore as,

$$C_a = \frac{C'}{C' + C_{1/2}} C_{sat} \quad (34)$$

in which C_{sat} is the space-averaged concentration of adsorbed solute in A at saturation and C' is the real free solute concentration in the pore, $C' = C/p$. If q_{sat} is the mass of solute adsorbed per mass unit of adsorbent, then $C_{sat} = q_{sat}d$, with d the apparent density of the adsorbent particles. In passing from Eq. (33) to Eq. (34), it is assumed that the concentration of free solute in the pores is equal to that in the external bath ($C'^{(eq)} = C_B^{(eq)}$), and the fact that the quantity of free solute may be neglected as compared to that of adsorbed solute.

If the initial concentration of solute in the batch adsorber, $C_B^{(0)}$, is sufficiently larger than $C_{1/2}$, namely in the plateau region of the adsorption isotherm, then the concentration of free solute in A in the vicinity of the surface of A will also be much larger than $C_{1/2}$ in the first moments of the experiment. Accordingly, the local amount of adsorbed solute will be nearly constant in that zone according to Eq. (34) because $C' \gg C_{1/2}$. Further away from the interface where the solute concentration drops to zero, the concentration of adsorbed solute will also become vanishingly small. However the flux of solute entering into a bead should be governed mainly by what happens near its surface, where the amount of adsorbed solute nearly does not vary with the distance. Therefore we may expect the present model to give satisfactory results when $C_B^{(0)} \gg C_{1/2}$, and as long as C_B remains sufficiently larger than $C_{1/2}$.

In the present study, a natural choice for the effective value of C_s was the value of the adsorbed concentration of solute at equilibrium for a representative value of the solute concentration in the

pores, C'_0 , that is,

$$C_s = C_a(C' = C'_0) \quad (35)$$

in which C_a is given by Eq. (34). A sensible choice for C'_0 is $C'_0 = C_B^{(0)}/2$ for a description of P varying between 1 and 0. Of course, this choice is not critical if $C_B^{(0)} \gg C_{1/2}$, in which case one then has $C_s \sim C_{sat}$ for any value of C'_0 .

3 Results and discussion

3.1 Description of experimental results

First, the accuracy of the analytical expressions derived assuming a QSS in the adsorbent was examined through comparison with results from finite-difference (FD) calculations in the case of constant external concentration. The FD algorithm was based on a diffusion-equilibration scheme used in previous work (Simonin *et al.*, 1988). The main result is that the QSS hypothesis is valid, and the analytical expressions are accurate, when $a \leq 0.1$.

Then, the results obtained in this work were applied to describe experimental results. The variation of the kinetics with the initial bulk adsorbate concentration and the validity of the predictions found in the theoretical section were examined. Kinetic data were found for various adsorbents, including chitosan (Wu *et al.*, 2001), resin (Hosseini-Bandegharai *et al.*, 2010), fly ash (Panday *et al.*, 1985), home made activated carbon (Demirbas *et al.*, 2008; Periasamy and Namasivayam, 1996; Santhy and Selvapathy, 2006) and commercial activated carbon (Kumar *et al.*, 2003; Choy *et al.*, 2004; Yang and Al-Duri, 2001, 2005).

The present model is not supposed to be applicable to systems in which ion exchange is the mechanism of adsorption because this process involves electric coupling between the diffusing ions. This is what we found when we analyzed for instance the data about the adsorption of Pb(II) in an algae gel (Vilar *et al.*, 2007). It was observed that P varied approximately as $t^{1/2}$ but it did not vary as $1/\sqrt{C_B^{(0)}}$. Actually it exhibited a non-monotonous variation with $C_B^{(0)}$.

On the other hand, satisfactory results were found in the case of experiments carried out with commercial carbon like Filtrasorb. Hereafter, we present an analysis of the data reported by Choy *et al.* (Choy *et al.*, 2004), and by Yang and Al-Duri (Yang and Al-Duri, 2001) about the adsorption of

two different dyes, acid yellow 117 and Cibacron reactive yellow F-3R (RY, molar mass $\sim 712 \text{ g mol}^{-1}$), respectively, in porous beads of activated carbon, Filtrasorb 400 (F400). The data of Yang and Al-Duri were particularly interesting because the main physical-chemical characteristics of the beads have been reported. Besides these results with Filtrasorb carbon, we present in the next section the result obtained in the case of the adsorption of Cu(II) on chitosan (Wu *et al.*, 2001) at short times.

The numerical values for the experimental kinetic measurements were obtained by digitizing the figures presented in the references.

3.1.1 Analysis of data at short times: variation of P with time and $C_B^{(0)}$

Experimental data may be represented using the approximate expression, Eq. (24) or (27), at short times, when the adsorption rate P is typically smaller than ~ 0.3 or 0.4 (Rudzinski and Plazinski, 2007, 2008).

It was first interesting to study the effect of varying the initial external concentration in (Choy *et al.*, 2004) and (Yang and Al-Duri, 2001). In these two references the initial bulk concentrations of the adsorbate were appreciably larger than $C_{1/2}$. One gets from Table 3 of (Choy *et al.*, 2004) that $C_{1/2} \approx 4.6 \text{ ppm}$, which is indeed much smaller than all initial concentrations $C_B^{(0)}$ that were in the range 50-200 ppm. In (Yang and Al-Duri, 2001), the values for a_L and K_L in Eq. (32) give $C_{1/2} = 1/a_L \approx 7.46 \text{ mg L}^{-1}$, which is much smaller than the values for $C_B^{(0)}$ that ranged from $\sim 34 \text{ mg L}^{-1}$ to 131 mg L^{-1} .

In the experiments of (Choy *et al.*, 2004), most of the values of the fractional uptake did not exceed 0.4, so that the approximate expression for P (Eq. (27)) was sufficient to analyze nearly all of the data. In (Yang and Al-Duri, 2001), the fractional uptake nearly reached its equilibrium value at the end of the experiments. Next, these data were analyzed here at short times and, besides, in the whole time range.

The results for the analysis of the fractional uptake P as a function of the square root of time are shown in Fig. 3 and Fig. 4.

The upper frames show the variation of P as a function of \sqrt{t} . The straight lines drawn for P smaller than ≈ 0.4 materialize the result of using the IPD equation at short times (Eq. (28)). These lines have different slopes so that the value of the IPD pseudo-diffusion coefficient, D_{IPD} , is observed to depend on the initial solute concentration in the batch

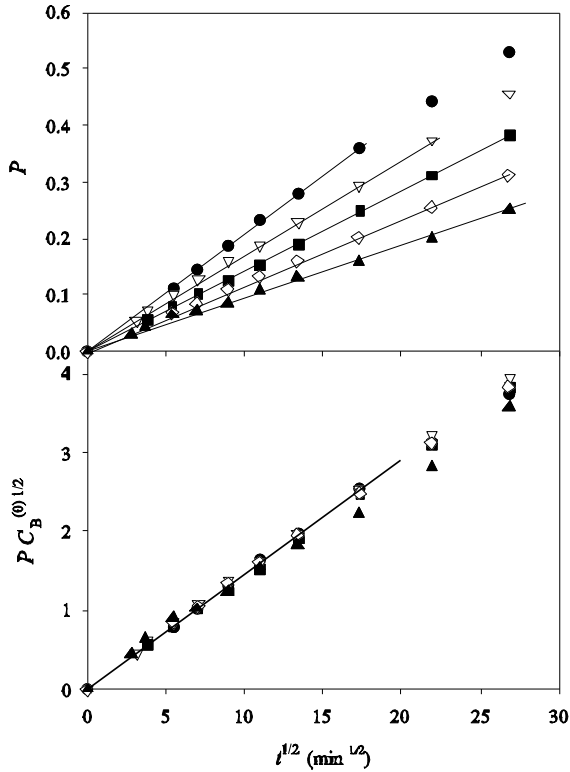


Fig. 3. Sorption rates as a function of time in the experiments of (Choy *et al.*, 2004) for various initial concentrations of solute in the bath. Upper plot: experimental values of P vs. $t^{1/2}$; bottom plot: experimental values of $P\sqrt{C_B^{(0)}}$ (in $\text{ppm}^{1/2}$ vs. $t^{1/2}$). Symbols: (\bullet) $C_B^{(0)} = 50$ ppm, (∇) 75 ppm, (\blacksquare) 100 ppm, (\diamond) 150 ppm and (\blacktriangle) 200 ppm. Lines: linear adjustments of points at short times (for $P < 0.4$).

adsorber, $C_B^{(0)}$. In Fig. 4, D_{IPD} is found to decrease monotonously from $\approx 1.3 \times 10^{-13} \text{ m}^2\text{s}^{-1}$ for the lower concentration ($C_B^{(0)} = 35.4 \text{ mg L}^{-1}$), to $\approx 0.61 \times 10^{-13} \text{ m}^2\text{s}^{-1}$ (for $C_B^{(0)} = 131 \text{ mg L}^{-1}$).

The bottom frames show the plots of the function $P\sqrt{C_B^{(0)}}$ as a function of \sqrt{t} . According to Eq. (27), this function is expected to be independent of $C_B^{(0)}$ if C_s is constant, which was the case for all values of $C_B^{(0)}$ because $C_B^{(0)} \gg C_{1/2}$. It is observed in the bottom frames of Fig. 3 and Fig. 4 that the experimental points for $P\sqrt{C_B^{(0)}}$ fall on a common straight line. So this result definitely points to a diffusion-controlled adsorption process in these experiments.

Besides these findings in the case of a commercial activated carbon (Filtrisorb), experimental data were analyzed in the case of other materials, spanning a

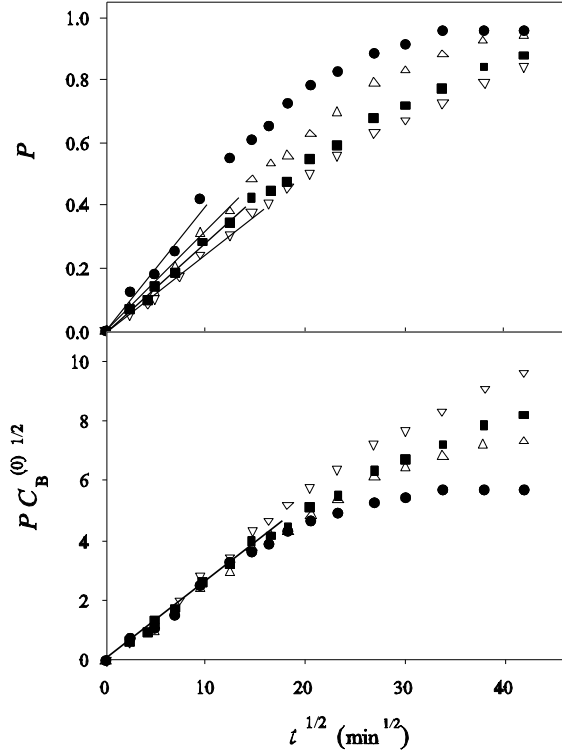


Fig. 4. Sorption rates as a function of time in the experiments of (Yang and Al-Duri, 2001) for various initial concentrations of solute in the bath. Upper plot: experimental values of P vs. $t^{1/2}$; bottom plot: experimental values of $P\sqrt{C_B^{(0)}}$ (in $\text{mg}^{1/2}\text{L}^{-1/2}$ vs. $t^{1/2}$). Symbols: (\bullet) $C_B^{(0)} = 35.4 \text{ mg L}^{-1}$, (Δ) 60.3 mg L^{-1} , (\blacksquare) 87.2 mg L^{-1} and (∇) 131 mg L^{-1} . Lines: linear adjustments of points at short times.

wide range of available sorbent types, namely for dyes and Cu(II) in home-made activated carbons (Demirbas *et al.*, 2008; Santhy and Selvapathy, 2006; Periasamy and Namasivayam, 1996); and for Cu(II) in a resin impregnated with an extractant (Hosseini-Bandegharai *et al.*, 2010), in a chitosan gel (Wu *et al.*, 2001), and in fly ash (Panday *et al.*, 1985). In most cases, the fractional uptake was found to vary as \sqrt{t} (or as $\sqrt{t}+A$, with A a constant) at short times (for $P \leq 0.4$) and to decrease with $C_B^{(0)}$, but it did not accurately vary as $1/\sqrt{C_B^{(0)}}$.

However, the case of the data for Cu(II) in chitosan (Wu *et al.*, 2001) gave an interesting result, which is shown in Fig. 5. The mechanism proposed in this reference (Wu *et al.*, 2001) for the adsorption of Cu(II) was the chelation by unprotonated amino groups of chitosan, without ion exchange.

Table 1: Values of input parameters in the model (in Eq. 17) for the data of (Yang and Al-Duri, 2001) for RY of molar mass $\sim 712 \text{ g mol}^{-1}$, and for which $R=0.0536 \text{ cm}$ and $C_{sat}=279.6 \text{ mol m}^{-3}$.

$C_B^{(0)}$ (mg L^{-1})	C_s (mol m^{-3})	a	ρ	λ
35.4	196.7	2.529×10^{-4}	0.08429	0.971
60.3	224.2	3.780×10^{-4}	0.1260	0.956
87.2	238.8	5.132×10^{-4}	0.1711	0.939
131	251.0	7.333×10^{-4}	0.2444	0.911

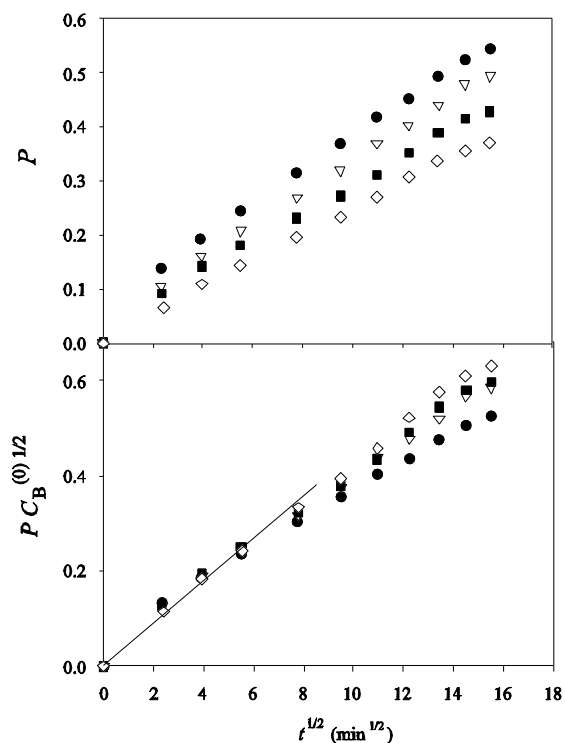


Fig. 5. Sorption rates as a function of time in the experiments of (Wu *et al.*, 2001) for various initial concentrations of solute in the bath. Upper plot: experimental values of P vs. $t^{1/2}$; bottom plot: values of $P\sqrt{C_B^{(0)}}$ (in $\text{mol}^{1/2} \text{ m}^{-3/2}$) vs. $t^{1/2}$. Symbols: (●) $C_B^{(0)} = 0.93 \text{ mol m}^{-3}$, (▽) 1.40 mol m^{-3} , (■) 1.95 mol m^{-3} and (◇) 2.92 mol m^{-3} . Lines: linear adjustments of points at short times.

It is seen in this figure that the experimental points for $P\sqrt{C_B^{(0)}}$ are fairly aligned on a common straight line. This result strongly suggests that the adsorption of Cu(II) was limited by diffusion in this medium.

3.1.2 Analysis of data in the whole time range

The experimental results of (Yang and Al-Duri, 2001) were also described in the whole time range by using the full equation, Eq. (17), together with Eqs. (19) and (23). For this purpose, the values of a and ρ were determined as follows. One gets the value of q_{sat} in Eq. (33): $q_{sat} = K_L/a_L \approx 199 \text{ mg g}^{-1}$, from which one obtains the value of C_{sat} in Eq. (34): $C_{sat} = 199 \text{ g L}^{-1}$ (with $d = 1 \text{ g mL}^{-1}$ (Chang *et al.*, 2004)). For each initial concentration, $C_B^{(0)}$, the value of C_s (Eq. (35)) with $C'_0 = C_B^{(0)}/2$ was employed to compute the values of a and ρ from Eqs. (5) and (9), respectively. The set of values for a and ρ is collected in Table 1. It is observed that a is always very small, smaller than 10^{-3} , so that the present model could be used because $a \ll 0.1$, as found from FD calculations.

Eq. (17), together with Eqs. (19) and (23), was used to calculate the concentration of solute remaining in the batch adsorber, C_B , as a function of time for various initial bulk concentrations. The value of D_0 was optimized 'manually' by plotting the experimental points together with the results from the model. The plots for C_B are shown in Fig. 6 for a common value, $D_0 = 5.83 \times 10^{-12} \text{ m}^2 \text{ s}^{-1}$ or $D = 1.08 \times 10^{-11} \text{ m}^2 \text{ s}^{-1}$ because of Eq. (6) with the value for the porosity, $p = 0.54$ (Chang *et al.*, 2004). We are not aware of any direct true diffusion coefficient measurements in porous carbon. However, some diffusivity values have been reported recently, that were obtained from the use of true diffusional models (not from the IPD equation): D of the order of $3 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$ for the fluoride ion in bone char (Leyva-Ramos *et al.*, 2010); of a few $10^{-11} \text{ m}^2 \text{ s}^{-1}$ for pyridine in activated carbon (Leyva-Ramos *et al.*, 2015) and for Rhodamine B in a zeolite (Castillo-Araiza *et al.*, 2015); and D in the range from $0.5 \times 10^{-12} \text{ m}^2 \text{ s}^{-1}$ to $27 \times 10^{-12} \text{ m}^2 \text{ s}^{-1}$ for various organic compounds in activated carbon (Leyva-Ramos *et al.*, 2012). Our value $D = 1.08 \times 10^{-11} \text{ m}^2 \text{ s}^{-1}$ therefore falls in the range of values obtained in these references. Besides, the diffusivity value of RY in bulk water should be of the order of a few $10^{-10} \text{ m}^2 \text{ s}^{-1}$,

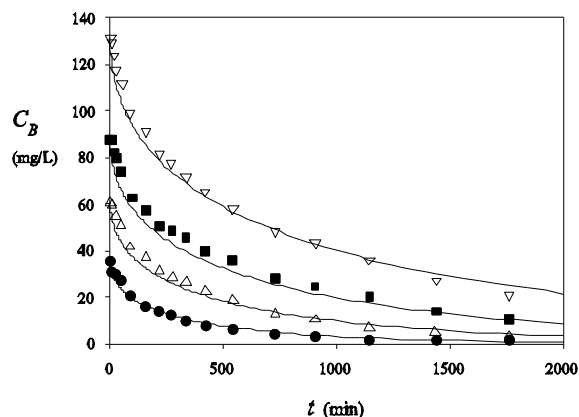


Figure 6: Concentration of solute remaining in the batch adsorber as a function of time in the experiment of (Yang and Al-Duri, 2001) for several values of the initial concentration and a diameter of 0.0536 cm. Symbols: (●) $C_B^{(0)} = 35.4 \text{ mg L}^{-1}$, (Δ) 60.3 mg L^{-1} , (\blacksquare) 87.2 mg L^{-1} and (∇) 131 mg L^{-1} . Solid lines: results for C_B obtained using Eqs. (17) and (22) with $D_0 = 5.83 \times 10^{-12} \text{ m}^2 \text{ s}^{-1}$ (see text).

as found by using the Stokes-Einstein formula ($D = k_B T / 6\pi\eta R$) at 25°C with a radius of the order of 8-10 Å for the solute molecule. Then, it is plausible that this value may be reduced by a factor of several tens because of effects due to tortuosity, and to confinement in the micropores which constitute the major part of the pores in F400 carbon (Chang *et al.*, 2004).

It is seen in Fig. 6 that the model gives results in rather good agreement with experiments for the 4 initial concentrations, with $C'_0 = C_B^{(0)}/2$, in view of the asphericity and polydispersity of the beads used in these experiments (Yang and Al-Duri, 2001). For the higher concentration of 131 mg L^{-1} , the agreement is satisfactory down to $C_B \approx 36 \text{ mg L}^{-1}$, which is ca. 3.6 times smaller than the initial value. For the lower concentration of 35.4 mg L^{-1} , the model gives a result for C_B that is in keeping with experiment at all times, even when C_B falls down to concentrations of the order of $C_{1/2}$.

The agreement with experiment is a little less accurate than that reported in (Yang and Al-Duri, 2001) in the framework of the branched pore diffusion model. However, this latter treatment involved 4 adjustable parameters instead of only one here (D).

Conclusion

In this work we have used an intraparticle diffusion-adsorption model to describe diffusion-controlled adsorption kinetics. It is expressed in terms of measurable physicochemical parameters. In principle, it is free of any adjustable parameter. However, the solute diffusion coefficient in the adsorbent must be available, which is generally not the case. Moreover, it is difficult to measure experimentally. Then D is the only unknown parameter.

An approximate solution was obtained for short diffusion times, which has the same form as the classical IPD equation, i.e. it varies as $t^{1/2}$. It has been shown that the diffusion coefficient introduced in the IPD equation is a lumped parameter. According to the present model, this pseudo-diffusion coefficient should decrease with the initial solute concentration in the bath, as the inverse square root of this concentration. Such a decrease has been observed experimentally in the literature.

The best adsorbents for the application of the present model are those in which the mechanism of sorption is not ion exchange. The model may be used when the external solute concentration is in the plateau region of the adsorption isotherm of the material.

At a more general level, it may be put forward that rate control by a chemical reaction is unlikely, especially in the (most frequent) case of sorbent particles of macroscopic size, in which complete adsorption takes an appreciable time (hours or sometimes days). On the other hand, limitation by a chemical reaction, or mixed chemical-diffusion control, may occur in the case of particles of small size in which diffusive transport may be fast (as e.g. in (Sharma *et al.*, 1990)). It should also be recollected that the best way to discriminate between chemical and diffusion control is to carry out experiments with beads of various sizes. Indeed, as underlined long ago by (Boyd *et al.*, 1947), the size of the adsorbent particles should have no influence on the uptake rate if adsorption is controlled by a chemical reaction, so long as the mass of adsorbent is kept constant. Furthermore, the shape of the particles should have no influence in this case, which is a very useful feature.

Acknowledgments

Fruitful discussions with Agnès Bée are acknowledged.

Nomenclature

Roman letters

a	$\equiv C_B^{(0)}/C_s$, dimensionless
a_L	Langmuir isotherm parameter, $\text{m}^3 \text{kg}^{-1}$
A	area, m^2
C	concentration of free solute, mol m^{-3}
C_a	concentration of adsorbed solute, mol m^{-3}
$C_B^{(eq)}$	mass concentration of solute in batch adsorber at equilibrium, kg m^{-3}
$C_B^{(0)}$	concentration of solute in batch adsorber, mol m^{-3}
C_S	concentration of adsorption sites, mol m^{-3}
$C_{1/2}$	mass concentration of solute in batch adsorber at which $q_a = q_{sat}/2$, kg m^{-3}
C'	mass concentration of free solute in pore, kg m^{-3}
C'_0	mean mass concentration of free solute in pore, kg m^{-3}
D	diffusivity of solute in sorbent, $\text{m}^2 \text{s}^{-1}$
D_{IPD}	IPD diffusivity of solute in sorbent, $\text{m}^2 \text{s}^{-1}$
D_0	effective diffusivity of solute in sorbent (Eq. (6)), $\text{m}^2 \text{s}^{-1}$
J	flux of solute per unit area, $\text{mol s}^{-1} \text{m}^{-2}$
K_L	Langmuir isotherm parameter, $\text{m}^3 \text{kg}^{-1}$
n	solute mole number, mol
p	porosity, adimensional
P	fractional uptake, adimensional
q_a	mass of solute adsorbed per mass of A, adimensional
q_{sat}	mass of solute adsorbed per mass of A at saturation, dimensionless
Q	quantity of adsorbed solute, mol
$Q_B^{(0)}$	quantity of solute in batch adsorber at $t = 0$, mol
Q_{IPD}	quantity of adsorbed solute in IPD equation, mol
r	radial coordinate in sphere, m
r_0	radius of shrinking core, m
R	sphere radius, m
t	time, s
v	volume of sphere, m^3
V_B	volume of solution, m^3
x	space coordinate, m
z	reduced radius $\equiv r_0/R$, dimensionless

Greek letters

δ	thickness of ash layer, m
λ	$\equiv (1 - \rho)^{1/3}$, dimensionless
ρ	maximum site occupancy ratio, dimensionless
τ	reduced time, dimensionless

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